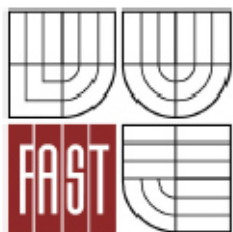




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FACULTY OF CIVIL ENGINEERING
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FOLDER No.7 Other calculations

Calculation of foundations

BAKALÁŘSKÁ PRÁCE
BACHELOR 'S THESIS

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a) LOADING OF THE MOST LOADED PERIPHERAL WALL

| HORIZONTAL CONSTRUCTIONS | TH. (m) | MASS (Kn.m-3) | LW (m) | SUM (Kn/m) |
|----------------------------------|--------------------|--------------------------|--|-----------------------|
| FOUNDATION SLAB | | | | |
| UNDER THE 1NP | 0,15 | 25 | 3,37 | 12,64 |
| FOUNDATIONS | | | | |
| (ESTIMATION) | 0,8 | 23 | 0,6 | 11,04 |
| CEILINGS | | | | |
| SLAB ABOVE 1NP | 0,25 | 25 | 3,37 | 21,06 |
| SUSPENDED CEILING ABOVE 2NP | | | | |
| KNAUF D 11 GYPSUM-BOARDS CEILING | 0,04 | 7,5 | 5 | 1,50 |
| ISOVER TOPSIL | 0,3 | 0,6 | 5 | 0,90 |
| FLOOR COMPOSITIONS | | | | |
| FLOOR AT THE 1NP a | | | | |
| FLOATING LAMINATE FLOOR PARADO | 0,007 | 3,9 | 3,37 | 0,09 |
| AFE 20 ANHYDRITE SCREED SAKRET | 0,04 | 20 | 3,37 | 2,70 |
| Isover EPS 100S | 0,15 | 0,25 | 3,37 | 0,13 |
| ELASTOBIT GG 40 | 0,004 | 12,25 | 3,37 | 0,17 |
| FLOOR AT THE 1NP b | | | | |
| CERAMIC TILES RAKO STONE | 0,008 | 22 | 0 | 0,00 |
| GLUE FOR CERAMIC TILES C1T SAKRE | 0,005 | 4,5 | 0 | 0,00 |
| AFE 20 ANHYDRITE SCREED SAKRET | 0,04 | 20 | 0 | 0,00 |
| Isover EPS 100S | 0,15 | 0,25 | 0 | 0,00 |
| ELASTOBIT GG 40 | 0,004 | 12,25 | 0 | 0,00 |
| FLOOR ABOVE THE 1NP | | | | |
| FLOATING LAMINATE FLOOR PARADO | 0,007 | 3,9 | 3,37 | 0,09 |
| AFE 20 ANHYDRITE SCREED SAKRET | 0,04 | 20 | 3,37 | 2,70 |
| Isover EPS 100S | 0,05 | 0,25 | 3,37 | 0,04 |
| ROOF STRUCTURE | | | | |
| WOODEN TRUSS | - | - | - | 2 |
| LATHS | | | | 0,2 |
| ELASTOBIT GG 40 | 0,004 | 12,25 | 7 | 0,343 |
| METAL SHEETS CORUS | | | | 0,35 |
| OSB | 0,025 | 1 | 7 | 0,175 |
| PERIMETER WALLS | | | | |
| HELUZ FAMILY 25 | 5,7 | 7,5 | 0,25 | 10,69 |
| ISOVER TOPSIL | 5,7 | 0,6 | 0,16 | 0,55 |
| WOODEN FRAME | 0,04 | 6 | 0,05 | 0,01 |
| WOODEN FASADE | 5,5 | 6 | 0,015 | 0,50 |
| SUM OF PERMANENT LOADS: | | | $\sum g_k =$ $g_d = \gamma g_k$ $g_d = 1,35 * g_k$ | 67,86 91,61 |
| VARIABLE LOAD | | | | |

| | LW | qk [KN.m ⁻²] | (Kn/m) |
|---|---------|--------------------------|--------|
| IMPOSED LOAD 1.NP | 3,37 | 1,5 | 5,06 |
| IMPOSED LOAD 2.NP | 3,37 | 1,5 | 5,06 |
| SNOW LOAD | | | |
| SNOW CATEGORY I. (VYSOKÁ NAD LABEM) | Sk= 0,7 | | |
| S = μ1 * Ce * Ct * Sk= 0,8 *1,0 * 1,0 * 0,7 = | | 0,56 | |
| | 7 | 0,56 | 3,92 |
| SUM OF VARIABLE LOADS: | | Σ qk= | 14,03 |
| | | qd=γ qk | |
| | | qd=1,5*gk | 21,05 |
| SUM OF ALL LOADING fd | | fd= | 112,66 |

SUBSOIL CONDITIONS:

ACCORDING TO THE TABLE FOR LOAD BEARING CAPACITY OF ROC (ČSN 72 1001)

R4, ROCK WITH LOW STIFFNESS

SYMBOL: R4 LOAD BEARING CAPACITY: $R_{dt} = 400 \text{ kPa}$

MATERIAL FOR FOUNDATIONS:

CONCRETE C20/25

$f_{ck} = 20 \text{ Mpa}$

PROPOSAL OF EFFECTIVE AREA:

$$b = f_d / (1 * R_{dt})$$

$$b = 124,44 / (1 * 400)$$

$$b = 0,311 \text{ m}$$

DESIGNED WIDTH OF FOUNDATION $b = 400 \text{ mm}$

$$a = (b - d) / 2$$

$$a = (400 - 250) / 2$$

$$a = 75 \text{ mm}$$

$$h = a \cdot \tan \alpha \quad \text{PLAIN CONCRETE } \tan \alpha = 1,5$$

$$h = 75 \cdot 1,5$$

$$h = 112,5 \text{ mm} \quad \text{MINIMAL HEIGHT OF FOUNDATION } h = 500 \text{ mm}$$

DESIGNED HEIGHT OF FOUNDATION $h = 900 \text{ mm}$ due to unfreezing depth

b) LOADING OF THE MOST LOADED INTERNAL WALL

| HORIZONTAL CONSTRUCTIONS | TH. (m) | MASS (Kn.m-3) | LW (m) | SUM (Kn/m) |
|--------------------------|------------|------------------|-----------|---------------|
| FOUNDATION SLAB | | | | |
| UNDER THE 1NP | 0,15 | 25 | 5,21 | 19,54 |
| FOUNDATIONS | | | | |
| (ESTIMATION) | 0,8 | 23 | 0,6 | 11,04 |
| CEILINGS | | | | |
| SLAB ABOVE 1NP | 0,25 | 25 | 5,21 | 32,56 |

FLOOR COMPOSITIONS

FLOOR AT THE 1NP a

| | | | | |
|--------------------------------|-------|-------|---|------|
| FLOATING LAMINATE FLOOR PARADO | 0,007 | 3,9 | 0 | 0,00 |
| AFE 20 ANHYDRITE SCREED SAKRET | 0,04 | 20 | 0 | 0,00 |
| Isover EPS 100S | 0,15 | 0,25 | 0 | 0,00 |
| ELASTOBIT GG 40 | 0,004 | 12,25 | 0 | 0,00 |

FLOOR AT THE 1NP b

| | | | | |
|-----------------------------------|-------|-------|------|------|
| CERAMIC TILES RAKO STONE | 0,008 | 22 | 5,21 | 0,92 |
| GLUE FOR CERAMIC TILES C1T SAKRE' | 0,005 | 4,5 | 5,21 | 0,12 |
| AFE 20 ANHYDRITE SCREED SAKRET | 0,04 | 20 | 5,21 | 4,17 |
| Isover EPS 100S | 0,15 | 0,25 | 5,21 | 0,20 |
| ELASTOBIT GG 40 | 0,004 | 12,25 | 5,21 | 0,26 |

FLOOR ABOVE THE 1NP

| | | | | |
|--------------------------------|-------|------|------|------|
| FLOATING LAMINATE FLOOR PARADO | 0,007 | 3,9 | 5,21 | 0,14 |
| AFE 20 ANHYDRITE SCREED SAKRET | 0,04 | 20 | 5,21 | 4,17 |
| Isover EPS 100S | 0,05 | 0,25 | 5,21 | 0,07 |

INTERNAL WALLS

| | | | | |
|-----------------|------|-----|------|------|
| HELUZ FAMILY 30 | 2,75 | 7,5 | 0,25 | 5,16 |
|-----------------|------|-----|------|------|

SUM OF PERMANENT LOADS:

$$\begin{aligned}\sum g_k &= 78,32 \\ g_d &= \gamma g_k \\ g_d &= 1,35 * g_k = 105,74\end{aligned}$$

VARIABLE LOAD

| | LW | qk [KN.m ⁻²] | (Kn/m) |
|-------------------|------|--------------------------|--------|
| IMPOSED LOAD 1.NP | 5,21 | 1,5 | 7,82 |
| IMPOSED LOAD 2.NP | 5,21 | 1,5 | 7,82 |

SUM OF VARIABLE LOADS:

$$\begin{aligned}\sum q_k &= 15,63 \\ q_d &= \gamma q_k \\ q_d &= 1,5 * q_k = 23,45\end{aligned}$$

SUM OF ALL LOADING fd

$$f_d = 129,18$$

SUBSOIL CONDITIONS:

ACCORDING TO THE TABLE FOR LOAD BEARING CAPACITY OF ROC (ČSN 72 1001)

R4, ROCK WITH LOW STIFFNESS

SYMBOL: R4 LOAD BEARING CAPACITY: R_{dt}= 400 kPa

MATERIAL FOR FOUNDATIONS:

CONCRETE C20/25

f_{ck}= 20 Mpa

PROPOSAL OF EFFECTIVE AREA:

$$b = f_d / (1 * R_{dt})$$

$$b = 124,44 / (1 * 400)$$

$$b = 0,311 \text{ m}$$

DESIGNED WIDTH OF FOUNDATION b= 400 mm

$$a = (b - d) / 2$$

$$a = (400 - 250) / 2$$

$$a = 75 \text{ mm}$$

$$h = a \cdot \tan \alpha$$

PLAIN CONCRETE $\tan \alpha = 1,5$

$$h = 75 \cdot 1,5$$

$$h = 112,5 \text{ mm}$$

MINIMAL HEIGHT OF FOUNDATION h= 500 mm

DESIGNED HEIGHT OF FOUNDATION $h=900\text{ mm}$ due to unfreezing depth